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NASA CONTRACTOR REPORT

NASA CR-137722

Copy Number

Vol. VI MARS System - A Sample Problem (Gross Weight of Subsonic Transports)

JULY 1975

Developed under CONTRACT No. NAS 2-7627

Multivariate Analysis, Retrieval, and

Storage System (MARS)

D.S. HAGUE

N.W. WOODBURY

Prepared by AEROPHYSICS RESEARCH CORPORATION Bellevue, Wash. 98009

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FOR THE NATIONAL AERONAUTICS AND SPACE ADMINISTRATION Ames Research Center, Moffett Field, California 94035

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PREFACE

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This report was prepared under Task II of Contract NAS2-7627,
"Further Flight Mechanics and Vehicle Synthesis Research", in the period
from June 1973 to May 1974. Mr. Michael J. Tauber was the NASA technical
monitor for this study which was done for the Advanced Concepts Branch
of the Aeronautics Division of National Aeronautics and Space Administration's
Ames Research Center. Mr. Donald S. Hague, of Aerophysics Research Corporation,
served as project leader for this study.

In the aerospace vehicle preliminary design process the estimation of subsystem component weights and costs are based on formulae obtained by multivariate correlation-regression analyses of historical data. While many groupings of such formulae have been presented in the past, there exists a need for a rapid method of verifying and improving these formulae in specific applications. The Multivariable Data Analysis, Retrieval, and Storage System (MARS) fulfills this function. In the MARS system selected vehicle characteristics information has been stored in a computerized data base. The data can be displayed, retrieved, or analyzed for functional relationships by multivariable statistical correlation-regression analyses using any specified subset of characteristics and vehicles.

This report, Volume VI of the Task II documentation, presents the detailed results for a typical aircraft wieght regression analysis. The particular example involves development of a gross weight estimation relationship for subsonic transport aircraft. The body of the report consists of actual computer printout.

INTRODUCTION

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The Multivariate Analysis, Retrieval, and Storage System (MARS) and its assc 'ated data bases of aircraft and engine characteristics has been described in References 1 through 4. Basically the MARS system is a tool for rapid prediction of aircraft or engine characteristics based on correlation-regression analysis of past designs stored in the data bases. Figure 1 illustrates program operation. Figure 2 illustrates the parts of MARS used in the present report. The present report is an example of output obtained from the MARS system. The example involves derivation of an expression for gross weight of subsonic transport aircraft in terms of nine independent variables. Independent variables for the example were:

 $L_{\rm p}$ = Body length, ft.

 $S_W = Wing area, ft^2$

 $D_R = Body depth, ft.$

 Λ = Quarter chord sweep, degrees

 S_{H} = Horizontal tail area, ft.

 $T_p = Root thickness, ft.$

 $S_v = Vertical tail area, ft²$

N = Ultimate load factor, "g"

AR = Wing aspect ratio

An expression for gross weight, W_{T} , was sought in the exponential form

$$W_{T} = a_{0} X_{1}^{a_{1}} X_{2}^{a_{1}} \dots X_{n}^{a_{n}}$$

Aircraft used in the correlation-regression analysis are listed in Tables I and II where the transport data base and its contents are listed. The resulting equation is:

$$W_T = 9.46 L_B^{-587} S_W^{-308} D_B^{-264} \Lambda^{-037} S_H^{-287} T_R^{-335} S_V^{-143} N^{-155} AR^{-111}$$

Note that the equation predicts that empty weight will fall with decreasing root thickness. This statistical anomaly reveals that thin wings have been more carefully (and expensively) designed than thicker wings rather than a true weight sensitivity to root thickness. This type of behavior is frequently encountered in "blind" statistical analysis. The example illustrates the need for careful selection of correlation variables and the need for continual review of the resulting estimation equations. There is also a need to have the ability to bound the variation of the coefficients to prevent such an anomaly. This last capability is now available in the latest version of MARS, Reference 5.

The remainder of this report consists of the actual computer output for the selected problem. The access-of-fit" obtained by the final equation is illustrated in Figur

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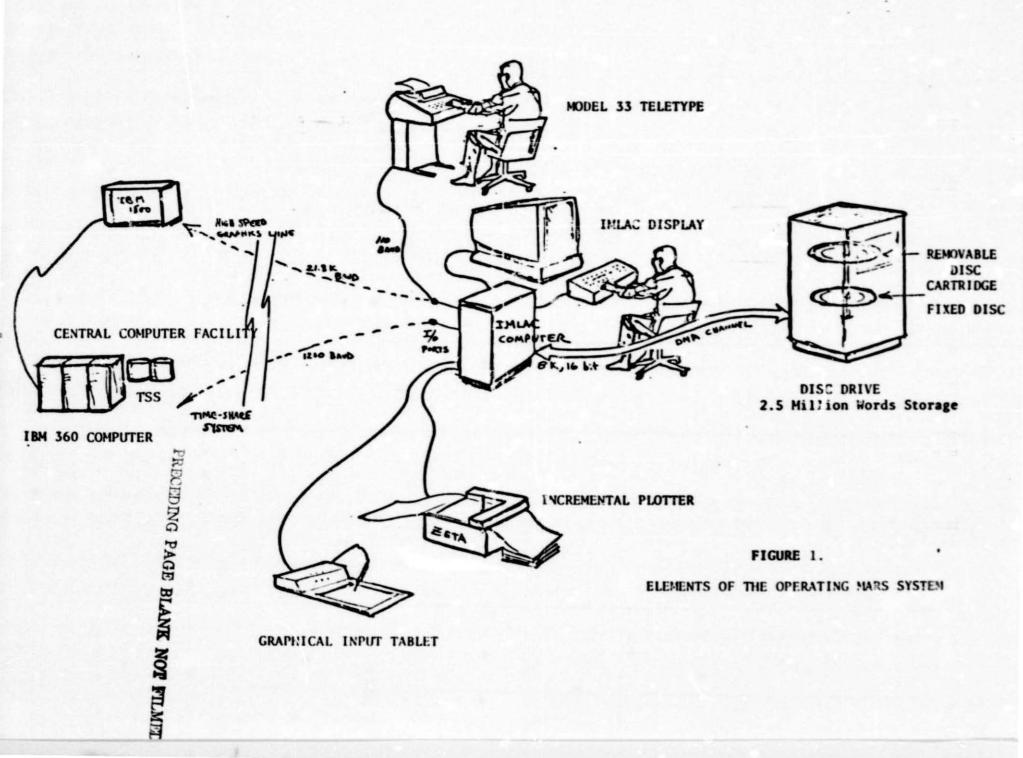
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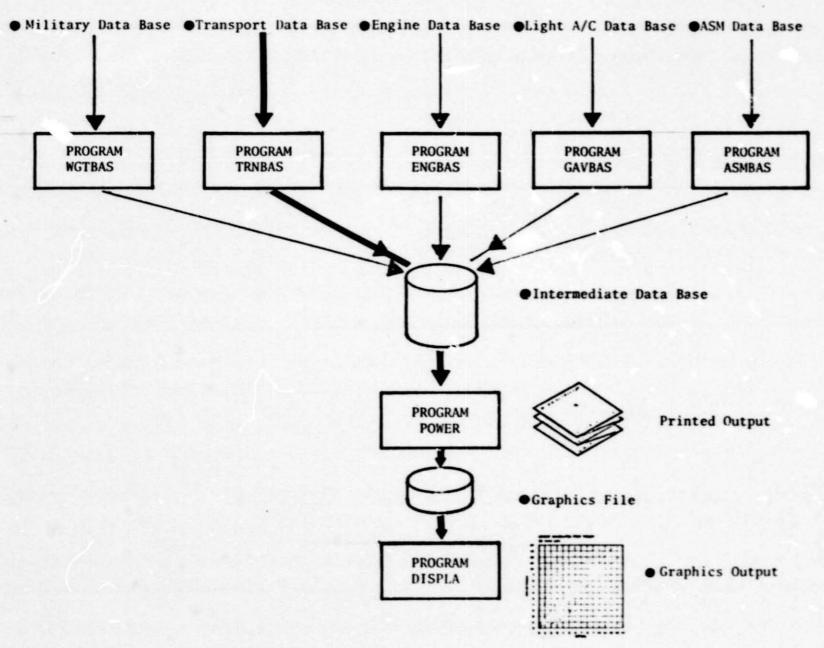


FIGURE 2. SCHEMATIC OF MARS PROGRAM OPERATIONS

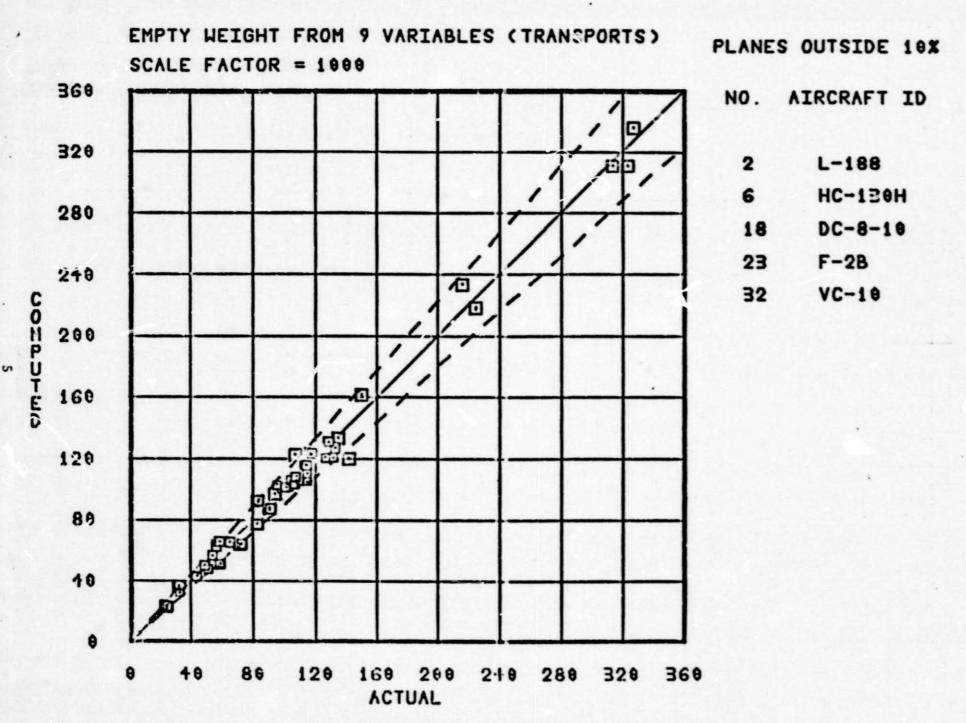


FIGURE 3. TYPICAL GRAPHICAL OUTPUT

TABLE I.

VEHICLES IN THE TRANSPORT DATA BASE, M2

1.	F-27	21.	880
2.	L-188, Electra	22.	990
	'C-130A	23.	F-2B
4.	C-130A	24.	DC-9-10
5.	C-130B	25.	DC-9-30
6.	HC-130H	26.	DC-9-30
7.	C-133A	27.	727-100
8.	C-133A	28.	727-200
9.	SE210-6N, Caravelle	29.	737-100
10.	707-120	30.	737-200
11.	707-020	31.	737-200
12.	707-320	32.	VC-10
13.	707-320B	33.	VC-105
14.	720	34.	G141-2
15.	C-135A	35.	C-5A
16.	KC-135A	36.	DC-10-10
17.	C-135B	37.	747-27
18.	DC-8-10	38.	747F
	DC-8F-54	39.	L1011
20.		40.	

TABLE II.

VEHICLES CHARACTERISTICS IN THE TRANSPORT DATA BASE, $\ensuremath{\text{M}^2}$

1.		49.	Furnishings Group Weight
2.	Design Load Factor	50.	Personnel Accommodations Weight
	Wing Area	51.	Personnel Furnishings Weight
4.		52.	Misc. Equipment Weight
5.	Wing Span	53.	
6.	t/c Root	7 54.	Air Conditioning Group Weight
7.	t/c Tip	55.	Air Conditioning System Weight
8.	Taper Ratio Ct/CR	rc	Do Ton Cuetam Maight
9.	Quarter Chord Sweep	56,	De-Ice System Weight
10.	Fuselage Length	57.	Number in Crew
	Euralana Mariaum Danth	58.	Number of Stewardesses
11.	Fuselage Maximum Depth	59.	
		50.	Number of Tourist Passengers
13. 14.	Tail Type Horizontal Tail Area	61.	Aileron Area
	Vertical Tail Area	62.	
15.	Action 1911 Mice	63.	Trailing Edge Flap Area
16.	Empty Weight	64.	Sint Area
17.	Sink Speed	65.	Spoiler Area
18,	Wing Group Weight	66.	Stabilizer Area
19.			Elevator Area
20.	Ming Secondary Structure Weight	- • -	Fin Area
21.	Aileron Weight	69.	
		70.	
23.			-
24.			Engine Make
25.	Spoiler Weight	72.	
		73.	
26.		74.	Inboard Nacelle Weight
27.	.	75.	Outboard Nacelle Weight
28.		76.	Fusclage Wetted Area
29.		77.	Inboard Nacelle Length
30.	Rudder Weight	78.	Inboard Nacelle Depth
31.	Body Group Weight	7ġ.	Inboard Macelle Width
32.		80.	Outboard Nacelle Length
33.	Alighting Gear Group Weight	81.	Outboard Nacelle Length
34.	Main Landing Gear Weight	82.	Outboard Nacelle Width
35.	Nose Landing Gear Weight		Total Aileron Area
36.	Surface Control Group Weight		Total Leading Edge Flap Area
37.		85.	Total Trailing Edge Flap Area
38.			
39.		86.	Total Slat Area
40.	A.P.U. Group Weight	87.	Total Spoiler Area
		88.	Maximum Dynamic Pressure
41.	Instruments & Navigation Group Weight	89.	Altitude for Maximum g
42.		90.	Maximum Mach number
43.	Hydraulic System Weight	91.	Cruise Speed Mach Number
44.	Procumatic System Weight	92.	Cruise Speed, Miles per Hour
45.	Electrical Group Weight	93.	Cruise Altitude
46.	Avionics Group Weight		
47.	Avionics Equipment Weight		•
48.	Avionics Installation Weight		
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                                      0.012547
       x 7
                   0.517101
                                      0.134252
                   0. *****
                                      0.171763
                   C. TISACA
                                      0.000219
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the or			
11111	0.954173		
 TO HEDR OF Y	0.372449		
-0111516	C.957469		
 	1.941		
VAPTAPLE	CCFFF 1C IFHT	STO. HIV. CF COFF.	
* 1	C.101700	1.100241	
	0.157054	0.155304	
	C.337845		
	-0.131945	3.090827	
* *		0.012614	
 ,,,			
	0.265179	0.178986	
 	0.106171	0.041359	
		the state of the s	

5110 NO. 9_		
ATOITALE EVALUIT		
E LEVEL	0.600624	
STO. FRACE OF Y	0.0/3379	
WULTIPLE R	C.993935	
CONSTANT TERM	2.247	
VAPTAPLE	CCECETCIENT	STO. SEA. CE COEF.
x 1	0.142969	3.114161
	0.15+251	3.15514?
* *	0.167910	0.034124
	-0.111105	2.143619
* *	-0.114066	1.103507
x.	0.036592	0.011095
* *	0.576551	0.149202

1.105614

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7-9-14-1 WILLIAM VIV. A. 0.422001 01

7,7444.74		FUSELAR	C TELETH, FLET		
5.MP41 40.	Winter In.	INDUT VALUE	CALCULATER VALUE	nirr.	WAT \$17
. 1	6-27	245 25. 523	0.330 AE UA	0.10110F 05	43.02 2
,	1.101	19912-031	P. 435794 Ch	0.551631 36	9.51 *
	C-1 134	57167.077	2.529751 05	-C 104. FF 04	-10.45 2
4	E-1 10A	47407.021	C. 42416F C5	-0.50/365 64	-0,61
	C-1304	1 14 19. 76.5	1.5599CE 95	-0.122 101 05	-14.14 E
A .	HC-113H	12514.061	E.FERECE CH	-0.16748F 25	-21.75 *
,	C-1734	114.413.363	0.143175 36	0.235011 05	70.17 *
	C-1344	113410.000	0.14017F CA	0.265/1F 05	21.14 1
2	54.21 3-64	50464. 177 1	J. 641 95 15	0.514745 94	9.65 *
10	717-120	164140.000	2.115745 00	0.590637 04	5.44 *
11	107-073	161400-200	3.10.351# 26	+0.13570F 04	-1.07 E
17	707-120	122600.000	2.1250ar Co	0.378035 04	2.18 *
11	107-1708	131563-125	2.125100 00	-0.44 TOSE 04	-4.17 T
14	722	101437.367	C. 10051F CA	-C.11178E C4	-1.10 K
15	C-1356	59357.763	3.975566 25	-0.180111 04	-1.41 \$
14	NC-1155	54103.344	C.STATCE CS	0.174 234 04	4.01 4
17	C-1350	105/10/1- 263	2.775565 25	-0.42441E 34	-7.79 7
1.4	00-9-13	106400.000	3.10939F CA	O. 3CARTE C4	2.89 %
17	95-FF-54	124169-000	0.12732F 06	-0.154105 04	-1.43 %
20	Df - R-6.2	134627.175	3.139675 06	0.505155 04	1.75 4
21	140	83014.053	3.907145 35	0.77200F 04	9.30 %
22	000	113520.175	G.10749F C#	-0.60367E 04	-5.32 *
**	F-28	31407.016	C. 170016 05	0.51155F 04	16.04 %
74	CC-9-1C	45890.027	U.48933F 05	-0. AGAGSE CS	-1.80 %
**	115-9-13	45247.017	J.AATRSE OS	0.11570F 05	20.04 5
76	00-9-30	55550.004	C. 64797E 05	3.1CR39E C5	19.17 \$
27	727-100	12797.000	9.719175 05	-0.104000 05	-13.14 %
21	727-200	90907.063	0.1097AE C6	0.18955F 05	20.74 \$
22	737-100	13400.023	0.472295 05	-J. 457CAF 34	-12.21 %
*1	737-200	*4828.027	0.443736 65	-0.50506E 03	-0.97 €
17	VC-12	141690.125	3.10563F 06	-0.360A2F 05	-25.45 E
23	VC-105	149800.125	2.23394E Ce	0.84143E 05	56.17 \$
14	G141-2	13360-125	0-10339E 06	-0.76975F 05	-20.69 \$

NO.	VEHICLE 10.	IMPLT VALUE	CALCULATED VALUE	DIFF.	FATIO
	F-5A	127302.125	3. 126115 06	-3.64531E 0	-0.71 E
5	00-10-10	224477.125	0.17474E CA	-0.40710F C	5 -27.15 \$
,	747-27	323073.253	0.313626 96	-3.12449F 0	5 -3.95 E
9	7475	313210.199	C.21042E 06	-0.25888F 0	-0.43 €
9	L1011	21599). 363	G.19035E G6	-0.25642E 0	5 -11.87 %
0	C-141-1	127640.063	C.1C338E C6	-0.24255E C	5 -17.00 E
	6	6 C-4A 6 CC-17-10 7 747-27 7476 9 L1011	6 C-5A 377007.125 6 CC-17-10 224477.175 7 747-27 373073.253 747F 313717.174 9 L1011 215693.363	6 C-10-10 224470.125 0.326715 06 6 CC-10-10 224470.125 0.174746 C6 747-27 323070.250 0.310426 06 7476 313210.144 0.210426 06 CL1011 215590.063 0.190356 06	6 C-10-10 224470.125 0.326715 06 -0.645315 0 6 CC-10-10 224470.125 0.174745 06 -0.407305 0 7 747-27 323070.250 0.310625 06 -0.124495 0 7 7475 313210.139 0.210625 06 -0.256885 0 1 L1011 21549.063 0.190355 06 -0.256825 0

	CARCELESTINAL	*********		VERTAGES			
				r LENGTH, FFFF			
1.171705			5A ,51007				
			M M.				
	SAMPLE NO.	VEHICLE ID.	TAPLE VALUE	CALCIN ATTE VAL 16	nite.		FATTO
	1	1-27	21576.633	3, 314" 01 25	0.747196	04	*1.41 2
	,	L-144	54012.0 1	0.541747 65	0.11/200	04	2.00 €
		F-190A	19112.321	0.6274.71 05	0.345495	34	A.C9 T
	. 4	f-120A	41407.327	0.A24641 05	0. 445775	64	0.44 T
	4	C-1409	47479.263	3.6476 31 35	-0.11114F	0+	-4.94 T
		HC-130F	12:33.363	2.647.05 65	-0. 770745	04	-10.43 7
	,	C-1314	116019-061	0.13177 GA	0.160.01	25	14.52 %
	4	C-1134	113012.263	C. 132771 C6	0.199596	CS	17.54 \$
		55113-64	\$8466.000	0.653845 05	0.751475	04	17.46 ₹
	10	7-17-179	101147.000	0.113755 66	0.541266	04	4.00 €
	11	107-220	101601.000	0.10412# 34	0.457 RF	04	4.45 1
	17	717-170	127469.303	0.171727 56	0.001526	C4	7.77 %
	11	717-1204	12156 3. 123	2.114*** 06	0.27000F	04	2.13 2
	14	120	101/30.063	J. 1061 7F C6	0.4.9386	04	4.47 *
	15	C-1354	54351.063	0.104925 06	0.406 HF	04	5.09 €
	16	KC-135A	54199.063	0.1046CF C6	0.105C1F	05	11.16 *
	17	C-1350	104001.063	0.104475 06	-0.13409F	04	-1.31 %
	10	05-8-10	106207.030	0.115454 04	0. 455066	04	*.10 *
	10	115-11-54	129143.000	0.137116 06	0.295 165	(34	7.20 %
	22	DC-8-62	1344 27.124	C. 14004F C6	0.541735	C4	4.07 %
	21	840	63014.063	C.904J1F 05	0.73H70F	04	8.90 €
	,,	5 +0	113123.125	0.195555 66	-0.70741E	04	-7.C2 T
	23	F-20	31 887. 316	0.345425 05	0.245246	04	#.32 E
	24	01-7-10	45.000.027	C.430718 C5	-C.49198E	04	-11.67 %
	25	00-0-30	54247.012	3.529626 35	-0.24083E	04	-4.36 T
	26	00-5-10	55553.004	3.5284CE C5	-0.309986	04	-5.47 \$
	27	727-133	£2797.233	0.719315 05	-0.10FOAE	4	-13.16 \$
	28	721-200	\$0000.063	C. 018365 C5	C.94567E	03	1.04 %
	29	737-100	41900.023	0.424505 05	-0.11750E		-21.10 \$
	31	757-200	54823.027	0.473456 35	-0.746276		-13.61 \$
	11	VC-10	141699-125	9.10704E 36	-0.344516	05	-24.46 \$

SAMPLE NO.	VEHICLE ID.	INPLT VALUE	CALCULATED VAL	LUF OIFF.		RATIO
14	5141-2	130360-125	0.1253AE 0	6 -0.5004AF	04	-1.84 \$
15	C-54	327001.125	0.331535 0	6 0.45295F	04	1.39 \$
34	20-13-10	224473.125	0.18339F OF	6 -0.41093E	05	-18.30 T
27	747-27	727273.750	0.301A3F 36	6 -0.21237E	05	-6.57 %
10	7475	317213.189	0.301435 00	6 -0.117776	05	-3.61 \$
10	11011	215000.063	0.190745 0	A -0.25630E	C5	-11.87 ₹
40	C-141-1	127643.363	0.12536F 06	6 -0.22845F	04	-1.79 \$



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EXPONENTION CONSTANTS			ANDIAGE					
1. 111000		55		Lincin, cert				
	1.451	74	WENT, AT	14.11				
	6.5416	*1	FUSFLAG	F WAX, PEPTH, FT				
9.								
540	mr we.	VIHICLE IN.	INCUT VALUE	CALCULATED VALUE	nitt.			AT100
	1	1-77	73574.C.3	2. 101000 00	0.460707	04		.01 1
	,	L-144	CAC12.031	0.41201F C5	-0. 19055	C.		. 74 *
-	•	C-1194	*******	3.6577AF 95	0.651.645	13%		.10 T
	4	C-1174	47407.927	0.44 1141 05	C. 71174.5	04		. 40 €
	4	C-11179	42674.063	5.66449F 95	-11.597941	-01		
		HF -1 100	126 34.GA 1	C.66990E C5	-0.50574	44		. 0.7 %
	,	C-173A	11/41 1. 043	1.13619F OA	0.19373F	0.	16	.50 T
		C-1374	117011.041	O. I TAI OF CA	0	65	19	.67 *
	•	SE 21 3-6"	57464-023	5.40757F 05	6.140136	04	,	.00 %
	10	707-110	108343.000	3.11155F CF	0.12110F	04	,	. 67 4
	11	737-020	101600.000	0.104425 04	0.381916	134		. 76 %
	12	101-120	122401.001	0.12549F C6	0. 1701 HF	.05	,	.69 %
	11	107-3708	121560-125	0.12819F OF	-0.337441	0.4	-2	. SA T
	14	720	101417.263	0.105625 06	0.378901	04	,	. 73 5
	15	C-135A	60 353.063	0.102377 06	0.13C41E	04	,	.03 1
	16	KC-135A	54107.063	C. 10251F C4	0.84126F	64	8	. 54 7
	17	C-1350	10 40 1.063	2.102375 00	-0.343201	04	3	.24 1
A. (8-year)	14	00-4-10	166803.000	0.109945 01	0.31440F	04	2	.94 8
	10	DC-4F-54	127140-000	0.122316 34	-0.624105	94	-4	. ** *
	20	DC-7-1.7	134420-125	0.129916 06	-0.571096	04	-4	.74 *
	21	693	63414-063	0.055415 05	0.252456	04		.04 1
	22	990	113523.125	C. 07225E 05	-0.167951	35		.35 %
	23	F-20	71 987. 614	0.357996 35	0.391224	24		.27 1
Sec. 1	24	00-9-10	45893.027	0.450415 65	-0.434946	34		. 77 %
	25	00-9-30	55267-317	0.5327eF 05	-0.199316	04		.61 *
	24.	00-9-30	55550.304	0.53276F C5	-0.26741E	04		.78 *
	27	727-100	e2707.000	U.731156 05	-0.95974F	2.		.69 2
	20	727-700	90500.063	G. 89327F C5	-0.15731F	04		.73 1
	20	737-100	12433.023	9.47179F 05	-9.65214E	04		.31 7
	31	737-200	14624.027	C.516344 C5	-0.319356	C4		. 02 %
	12	VC-10	141690-125	.1054DE 06	-0.3A293F	05		.47 1
	4.6				*******			

SAPPLE NO.	VEHICLE ID.	TOPUT VALUE	CALCULATED VALUE	DIFF.		PATIO
**	VC-175	140003.125	3.16577E 06	0.159 1AE	25	10.67 \$
14	6141-7	130160.125	C. 12046F C6	-0.040BRE	C4	-7.79 *
15	(-5A	22700 1. 125	0.381628 06	0.546716	05	16.70 \$
36	00-10-10	224471.125	0.15783F C6	-0.76617E	CS	-11.67 3
17	747-27	3. 3070.250	3. 31 3565 CA	-0.35075E	04	-1.09 \$
10	7475	*13212.189	G. Plaser Ce	0.63576F	C4	2.03 %
20	11311	215593.363	0.203A15 06	-0.12183F	35	-9.73 \$
40	C-141-1	127649.063	G. 120PAE C6	-0.67738E	C4	-5.31 %

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771-141 WEITING W. A. 0.1-427 D.

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CUSCINCE LINEIN, FIFT WING ASSAULTER? FUSCINOS MAK, ELPTH, FT ELSTE (WING , 25 CHOSE LINE)

SAMPLE NO.	MINICIF IF.	INDIST VALUE	CALCULATED VAL			PATTO
,	1 . 27	235 25	0.274.77 34		04	17.27 %
	1-17#	*4717.391	3.51 1576 05		04	-11,99 \$
	C-1774	50167.327	Gandanas no	0.245.05	C4	4.70 T
	C-1174	41421.021	0.414117 05	6.490-45	04	4.94 1
4	E-1703	67573.263	0.175000 05	-0.507676	04	-7.51 %
	FC-135H	124 114 361	0.625 (25 05	-0.35 W 2F	04	-13.24 %
7	C-1314	116917.069	2.114.75 04	0.153435	C4	1.55 €
•	C-1111	11 101 1. 36 1	0.114477 36	0.4447	34	4.CO T
	56 21 0-64	\$5466.021	. C. 61 30 45 C*		04	5.01 %
12	737-170	16814 1. 131	0.114526 66	0.417734	04	4.70 \$
11	707-320	101/01.077	C. IGHTER CO	0.0774.25	0+	#.15 T
12	707-370	127/43.003	0.123741 04	. 0.61567F	04	4.32 \$
11	107-1701	1315/ 9-125	3.1*1145 04	-0.270755	C3	-0.17 ·
14	723	161/11.063	3.120*45 04	0.074415	04	4.11 *
15	C-135A	60259.363	0.10.74F C	0.71975F	64	7.41 1
10	KC-1350	C4107. 261	3.1U685F CA	0.127535	05	13.55 \$
17	C-1358	105807.063	0.10674F C	6 0.9-150F	03	0.89 \$
14	36-8-13	106*03.000	0.117152 16	0.444.35	04	5.70 \$
10	OC-0F-54	129140.000	3.12413F C	-0.50 TA	04	-1.91 1
*0	05-9-67	124620-124	C. 128835 96	6 -3. 773945	04	-4.30 E
21	PAC	#3014.061	0.881705 05	5 0.5155RF	04	6.21 T
2.	990	11312:-125	0.5874 \$ 05	-0.1.779F	05	-13.02 4
73	F-20	31887.016	C. 77547E C5	5 0.50553F	04	17.74 %
74	DC-0-10	44 80 7. 027	0.477235 35	-0.24649F	04	-5.35 %
75	05-6-30	55269.717	C.54058F C5	-0.17109E	C4	-7.19 T
76	00-9-30	*444 1. 034	G. 5405AE 05	-0.10019F	04	-3.36 E
27	777-100	A2707.330	0.76971F C*	-0.54241E	C4	-7.01 T
70	727-730	50907.063	0.995A1F 05	-0.111476	04	-1.47 \$
20	737-100	\$1801.023	0.503528 05	-0.34485F	C4	-6.4: 1
*1	737-21 0	54624. 327	3.543545 05	-0.47418E	03	-0.96 \$

SAMPLE .	C. VEHICLE ID.	INPUT VALUE	CALCULATED VALUE	DIFF.		PATTO
12	Vr-10	141493.135	0.108*25 06	-0.120345	05	-73.77 %
31	VC-1C5	144 800.175	C. ISASTE CA	0.71774F	04	4.79 1
14	6141-2	110103.125	0.125146 06	-0.51799E	04	-3.97 E
35	C-54	327300.125	0.37945E CA	0.574506	C5	1610 €
**	06-10-10	224473-125	2.233745 06	-0.23506F	05	-9.14 %
17	747-27	323073.250	0.71760F C6	-0.51775E	04	-1.66 %
10	7471 ~	211210.193	J. 31 759F 06	0.444766	04	1.43 \$
32	LICIL	214591.061	0.20750F C6	-0.840A6E	04	-3.49 %
40	C-141-1	127443.943	0.1251 AF 36	-0.24598E	04	-1.93 %

TRANSPORTER TON LORD WITCHT. POUNDS

1 10	rantine.	CENSTANTS		VARIABLE			
1.6.155.13		FUSCIALI LENGTH, FEET					
	(. 1714		41115 74	13,17017			
	C. 1635		THE ! AC	WAX. DEPIM.FT			
.1	1.75.7		£ 2511 T B	WING . 25 CHEEF LINE	1		
	1, 1416		MORTH.	"L TAIL APIA, FIFE?			
***	115 117.	WENTER IN.	INPUT VALUE	CALCULATED VALUE	nier.		PATER
	1	1-11	28574.677	0.263.77 05	0.27100	04	11.56 7
	*	1-1-4	50012.711	3.457121 05	-3. ATE 6.41	04	-14.11 1
		C-110A	49162.977	0.635251 (5	0.446346	C4	7.39 *
	4	C-130A	57407.027	9.417197 45	0.438125	94	7.67 1
	•	C-1300	67578.C63	0.44 4711 65	-0.370771	64	-4.75 *
		HC-13 H	72637.063	0.44077 04	-3.794075	04	-11.02 \$
	,	C-1375	116810.003	0.112226 66	0.240646	34	7.C6 T
	1.00	C-123A	112812.263	0.110245 06	0.54110F	04	4.17 K
	140	55210-64	58465.023	0.41135 65	0.247765	04	4.57 \$
	1.0	737-170	1C#140.000	0.112905 06	0.454146	94	4.21 €
	1:	107-620	101400.000	0.1CP52F C*	0.402095	04	6. *1 T
	17	737-120	12260 1. 023	0.131341 06	0.474135	94	7.16 \$
	11	101-3/64	121560.125	0.137345 C6	C. 17980E	C4	1.17 7
	14	120	101/30.063	0.108525 06	g.agegor	94	6.78 X
	15	C-125A	\$0357.063	0.10436F C#	0.70016F	C4	7.05 7
	11	KC-135A	54100.042	0.106-75 34	0.123/46	05	13.14 *
	17	C-1350	105807.CA3	0.10973F CA	0.247486	64	7.77 *
	1.9	05-4-13	164+63.033	9.114497 96	0.74.0016	04	7.20 1
	14	DC-8F-54	127160.000	G. 12445E 06	-0.450926	C4	-1.49 2
	20	DC-8-62	134/23.125	0.174795 36	-0.462701	04	-4.18 T
	21	880	63C14.GA3	0. P7470F C5	0.445/15	34	5.17 X
	2"	200	113523-125	0.092745 05	-0.15294F	05	-13.47 \$
	23	5-24	21867.016	C. 3671 PF C5	0.483606	04	15.15 \$
	74	00-9-10	45,893.027	0.477155 05	-0.217456	04	-4.16 E
	29	00-9-30	55269.012	0.539176 05	-0-111104	04	-7.41 %
	7.	PC-7-13	55550.034	0.539376 05	-0.201206	04	-1.60 \$
	21	727-100	#2797.000	C. 76059F 05	-0.677896	C4	-8.13 *
	27	727-200	90907.063	0.876628 05	-0.123796	34	-3.56 E
	20	737-100	13000.073	0.5C947E 05	-0.28511F	04	-5.10 \$

SAMELE NO.	VEHICLE 10.	INPL. VALUE	CALCULATED VALUE	DIFF.	PATIO
21	737-200	\$4827.027	C. 5446 SE OS	-0.343436	03 -0.66 \$
11	VC-10	141693.125	0.114426 06	-0.25770F	GS -18.89 T
17	VC-1C5	140 80 3-125	C.15058E CO	0.079136	04 6.53 5
74	6141-2	130363-125	0.117945 06	-0.12403E	05 -9.51
**	1-54	327000.125	0. 12 172E C6	-0.32825F	C4 -1.00 T
16	20-10-10	224473.125	0.221566 14	-0.29143F	04 -1.30 1
**	747-21	223070.75C	0.72455F C5	0.147945	0.46 1
19	7475	213210.134	0.324556 0	0.11340E	25 3.62 1
12	11011	215993.061	0.223156 0	0.74C3RE	C4 3.41 1
40	C-141-1	127643.363	0.1179ef 36	-0.968246	04 -7.59 1

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TRUSTON WEITHER VIS. A. C.P. P. C.

MONITORAL CENSTANTS	VAPIAPLE
6.517.67	EUCHLAGI LEWITH, FFFT
C. 105074	4176 ## (1,174.)
f. 13739C	COSPLACE MAK. DEPTH.FT
0.312290	coster twins .25 Comp Link
C. 1745.54	HENT PERAL TALL APPA, FT
-6.147714	TIC AT ROOT
	0.101024 0.107290 0.512290 0.124614

	NO. VINICIE IO.	INPLT VALUE	CALCULATIC VALUE	niff.		PATIO
	1-37	2157- 610	0.233116 05	-0.7476 1F	07	-1.11 *
,	1-144	54011.031	0.517216 65	-C. 678845	C4	-10.44 1
	C-135A	52142.027	4.6 42 74F 35	0.411216	04	4.64 *
	C-1324	574 37.027	0.421567 65	3.474916	64	8.27 T
4	C-1125	671 79. 54.1	3.64755F A5	-0.26196F	04	-1.00 %
	HF-130H	72034.063	0.546385 65	-0.743025	04	-10.11 *
7	C-133A	115#1 1. 263	2.120156 06	0.333946	04	2.44 \$
1	C-1330	113813.363	0.120100 04	0.437176	54	5.60 1
2	55 213-69	50464. 323	0.63676F C5	0.521026	24	# .91 T
13	707-120	108749.090	0.10753F Cf	-9.80750F	13	-0.75 \$
11	757-370	161400.711	0.104145 06	3.757675	04	2.44 %
12	701-323	122600.000	0.12/ 935 06	0.420096	04	1.41 *
1.	707-3208	131567-125	0.120026 05	-0.27401F	34	-7.08 T
14	776	1614 27.063	0.104100 06	0.254666	94	2.51 5
15	C-135A	59359.063	0.100595 04	0.171415	04	1.21 1
16	KC-1354	54103.063	0.100665 06	0.455736	C4	4.97 *
17	C-1358	103802.343	J. 10343F 06	-3.23666F	04	-2.74 E
1.4	00-4-10	164900.000	0.121535 00	C.14#79E	CS	13.49 #
19	11C-AF-54	127169.000	0.129456 06	0.285698	03	0.27 %
20	"C-8-67	134620-125	C. 13374F OA	-0.13843F	04	-1.23 1
21	890	43014.043	0.004655 05	3.745C9F	04	#.9* T
22	990 -	113520.125	0.103975 C6	-0.95491E	04	-8.41 %
**	F-29	71 007. 716	0.362045 05	0.43166F	04	13.54 \$
74	20-9-13	45 393. 027	0.456375 05	-0.75140E	63	-0.51 \$
25	DC-9-30	55767. 312	0.542295 05	-0.10+04F	34	-1.44 8
26	00-0-30	45550.204	0.44279E C5	-0.17714E	54	-3.CA T
27	727-130	62757.000	0.732745 05	-0.94228E	04	-11.50 E
28	727-200	50000.063	0.675996 05	-0. 33010F	04	-3.63 *

	SAMPLE	NO.	VEHICLE IT.	INPLT VALUE	CALCULATED	VALUE	CIFF.		RATIO
	29		737-100	53000.023	0.473396	C5	-0.14114F	04	-2.67 X
	11		737-200	54F29.327	0.440015	05	0.114285	04	7.12 \$
-	**	-	VC-10	141493.125	0.119876	CA	-0. 21 P19F	05	-15.40 \$
	**		VC-105	140000-125	U.14977F	CA	0.04744€	04	6.32 \$
	34		5141-7	130360.125	0.121955	Ch	-0.840*3E	**	-6.45 1
	75		C-5A	127003-125	0.336626	06	0.067735		2.94 1
	14		05-10-10	214470.125	0.21764E	Ct	-0.68*44E	04	-1.04 \$
	17		747-27	123073.250	3. 328735	06	-0.143375	05	-4.44 1
	39		7475	313213.188	0.303736	CA	-0.44771E	C4	-1.43 %
	19		11011	215997.043	0.214925	Oe.	0.18829F	05	8.72 \$
	40		C-141-1	127443.063	0.12195F	Ce	-0.56873E	C4	-4.46 \$

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4 - 4 4 41 .					
Cart I			LINGTH, FEFT		
(. 144	100		1 1.1.1002		
	**		TAK. CEPTH, FT		
6.0457	14	*353*14	-156 .75 Came 11cf	1	
*. 3156	**	141 10 1 154	THE TALL APER, FT 1007		
-6.1473	144	1/1 11	0.1.17		
	41	VC TICA	L TAIL APPA, FT.		
SAMPLE WIL	VEHICLE IC.	INPLY VALUE	CALCULATED VALUE	nirr.	PATIO
1	1-7"	235 74. 203	6.234 167 35	-0.13050F 0	· -J.59 #
,	L-144	54017.031	0.5007/# 35	-0.717541 0	4 -17.17 \$
,	C-130A	50167.027	0.639455 35	0.479341 6	4 H.CO T
4	C-110A	47407.027	Q.61447F 35	0.444.045 0	4 7.77 *
	C-1 50%	67479.043	GARAGRAF CS	-0.29521F C	4 -4.17 *
4	140 -1 1514	12633.063	J. 642 *3F 25	-0.77555 0	· -10.77 T
,	C-1334	116819.063	0.122125 06	0.511146 0	4.15 *
	F-1 114	113913.353	0.122165 36	0.8345AF C	4 7.31 1
9	5F210-4N	54444.773	C.4.1051F C5	0.450515 0	4 7.85 *
1.1	7:17-17:3	1(474).00)	0.10-345 0/	-0.15050E 0	4 -1.39 Z
11	737-220	101/02.022	0.103506 56	0.100796 0	4 1.07 %
12	707-120	122403.000	0.125807 06	0.320356 7	4 2.61 %
11	707-3209	131560-125	C-12745F CF	-0.39079F C	
14	723	101/30.063	0.103695 56	0.235146 0	
15	C-135A -	66159.061	C.10125f 06	0.174491 0	
14	*C-1354	94107.367	0.10054F CA	0.443518 0	4 6.44 %
17	C-135"	105803.063	G.10408E Go	-0.171 COF C	
10	00-8-10	164767.007	0.122196 36	0.15390# 0	4 14.41 T
19	CC-4F-54	129160.000	0.120525 06	0.45/31F C	3 0.35 *
20	110-11-12	134/23-124	0.123356 06	-0.12697E J	4 -0.94 E
21	990	£3014.063	C.91374E C5	0.829036 0	4 9.99 7
22	590	113527.125	0.134565 06	-O. REALSE O	4 -7.89 \$
23	1-24	21987.014	0.350575 C5	0.40# TOF 0	4 12.76 2
74	00-9-10	49893. 027	0.494247 05	-0.40429F d	3 -0.41 %
25	00-9-10	55267.012	0.539191 05	-0.11107E 0	4 -2.41 8 _
26	nc-9-30	55650. 304	3.430300 05	-0.23112E 0	4 -3.59 \$
27	727-10C	e2797.00C	C. 74910E 05	-0.79870F C	4 -9.53 %
27					

SAMPLE NO.	VEHICLE ID.	INPLT VALUE	CALCULATED VALUE	DIFF.	RATIO
22	727-200	90000.063	0.369135 05	-0.198745 04	-4.19 \$
20	737-100	53000.021	0.579235 05	-0.87710F C3	-1.43 8
21	737-200	54828.C27	0.56.4ngF 05	0.16411E C4	2.49 €
17	VC-10	141697-125	0.123A3E 36	-0.21UACE 05	-14.86 %
12	VC-105	147/07-124	0.159707 56	C. 91997E 04	6.27 %
14	6141-2	130343-125	C-127656 06	-0.770#6F 04	-5.01 %
35	F-56	327300.125	C. 33462F C6	0.76191E C4	2.13 %
71	00-10-10	224473.124	3.21710F GA	-0.74730F C4	-3.13 \$
37	747-27	223371.250	0.200171 06	-0.14901E 05	-4.61 *
39	7476	312210-198	0.303176 06	-0.50413F 04	-1.61 %
10	11011	215653.063	0.23315E C6.	0.171595 35	7.94 2
43	C-141-1	127640.003	0.122n5E 06	-0.49FR6E 04	-3.91 €
	16.475	The second secon			

Express 115A	I CENSTANTS		VAPIABLE				
11.571	710	FIRSTLAS	t treate, cert				
1.111			F4.F1147				
1. 345			. MAR. PIRTH. FT				
		CHEISTE	1141 .35 CHOOM !	1853			
0.474			SL TALL ADTA.FT				
+(.11)		1/6 11					
0.191		7.5	L TAIL ANTA.FT.	• ?			
* ****			I LOSE PACTUR.				
CAMPLE 117.	VERTER IC.	INPUT VALUE	CALCULATED VA	tur nirr.		MATIO	
,	1-27	*** 74. 503	0.226106 3	0.140156	97	0.14 %	
2	1-109	52012.031	7.43449F 0	-0.756275	134	-11.04 €	
1	C-1170	59162.027	0.444500 0	5 0.5591.45	C4	9.63 4	
4	C-130A	47407.327	0.62839F 0	3.540256	34	7.41 4	
•	C-132"	67478.C63	0.448416 6	-0.273716	C4	-4.05 5	
	117-13711	77514. 267	J. 64511E 3	-3.7476.95	04	-10.45 7	
.,	C-131A	114910.063	0.121975 4	0.714716	04	6.11 5	
	C-177A	113013.263	0.11A49F 0	0.24*716	24	2.15 \$	
9	56710-A"	*#465.023	0.125036 0	5 0.40770F	C4	6.90 %	
1.5	707-120	104343.300	3.10645E C	-0.140245	04	-1.38 *	
11	101-627	161602.000	0.103136 0	. 0.15734F	04	1.*1 *	
12	707-323	172+00.303	3.1255AE C	0.295018	04	2.41 %	
13	707-1204	131563.125	0.12727E C	-0.420415	04	-1.26 *	-
14	723	101/30.063	3.103436 3	0.143315	04	1.77 *	
15	F-135A	59357.063	0.101695 0	6 0.23376E	04	2.35 %	
16	KC-1355	54100.063	3.971275 0	0.102715	04	3.22 %	
17	C-1354	105800.363	0.10441F C	e -0.1391eE	04	-1.72 *	
1.0	05-5-10	104900.000	J. 1221 75 J	0.153726	05	14.39 \$	
19	115-6F-54	120160.000	0.179176 C	e 0.711CAF	03	0.55 *	
20	20-9-47	134620-125	0.133915 0	-3.73443F	03	-0.52 %	
21	*40	£3014.343	0.917245 0	5 0.871C4E	C4	10.49 %	
27	990	113522-125	0.10503F 0	-0.85152F	04	-7.50 T	
23	F-28	71887.014	C. 35593E C	5 0.360596	04	11.59 8	
**	00-9-10	45893. 327	3.49994F 3			0.21 *	
25	CC-9-30	55769.012	0.53904E C	-0.13650F	C4	-2.47 E	
26	DC -4-30	55553- 034	3.53934F G	-0.20450F	34	-3.66 E	

SAMPLE MO.	VEHICLE IN.	INPLT VALUE	CALCULATER VALUE	olff.	RATIO
27	727-100	P2797.000	0.757065 05	-0.70012F 04	-R.56 T
24	727-200	50°00.043	C. 97177F Q5	-0.17776F C4	-4.15 *
26	717-100	51000.023	9.52724F 05	-3.10719E 04	-1.99 %
31	737-200	14074.327	0.563146 65	0.1556 TE C4	2.84 E
12	VC-12	141493.175	0.123416 36	-0.21076F 05	-14.27 2
11	VC-105	145 800.125	7.1610.5 06	C.17104F 05	8.C5 T
14	G141-7	130343.125	0.122545 06	-0.79173F 34	-6.00 %
16	C-54	227:00-125	3. 23561F Ce	3. P6009E C4	7.43 %
*6	00-10-10	224473-125	0.214175 06	-0.83034F 04	-3.70 %
37	747-27	223077.250	C. 71050F C6	-0.124 CE CS	-3.86 %
**	747F	212712-199	C. 31050F C6	-0.76176F 04	-0.84 T
3.0	L1011	215590.063	0.23160F 06	0.15611F C5	7.23 1
40	C-141-1	127640.063	C-12254E G6	-0.53492E 04	-3.99 T

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(parket elect	CASTARTS		V*******			
1.5000		fusti at	e truning ffff			
		W195, #F				
1.7741		11151175	. WAT. IMPTH.FT			
	**	* 15110 *	with . w. forth Lines			
1. 1711		16.141756	AL TALL PULA, FT			
		1/5 /1	1010			
. 1.1475		VI 0 11C/	L TAIL APIS, FT			
r.1547		1/1 71 ****	Lata Intine. C.			
** . 1111	***	W185 15	PECT SETTE			
	WENTELF IT.	INDIT VALUE	CALCULATED VALUE	mer.	*****	
	1-17	*1575.500	U. 774-46 55	-3.03504 00	-0.14 1	
1	1-100	10017.011	G. *16:06 CS	-7.000 105 64	-15.45 4	
,	C-1334	55167.027	3.446. FEF 05	0.551355 34	2.77 *	
	f-130A	* 1401.021	C. 67 /50F CS	0.531777 54	9.75 7	
- 4,	f-11.00	(7574.C53	7. *** TAF C*	-5.200711 04	-4.29 \$	
4.	per - 1 100	7*011.061	7. 1. 4 * 1. ar C*	-7. 7A7-5F C4	-10.44 *	
,	F-1114	111 213. 213	1.17327 06	3.440701 04	5.40 E	
	C-1111	117717.0A7	0.115 FFF CA	0.176541 04	1.73 *	
•	e10-14.	4.444.371	0.416175 05	0.115135 74	5.10 \$	
10	707-120	104141.710	0.136 157 64	-0.159661 64	-1.47 7	
11	737-676	1616-52- 333	3.107 746 04	0.13444F 04	1.72 1	
17	707-770	122/01.010	0.124755 CA	0. 210275 54	1.79 *	
11	777-37-9	1 *1 50 1.12"	0.17446 26	-0.577175 06	-7.97 \$	
14	723	101/10.041	O.ICITAF CA	0.171che 34	1.70 €	
15	r-1754	64140.041	G. 1::7246 OF	0.287AR* 04	2.90 %	
14	#C-1154	54100.063	0.971406 65	0. 13501F C4	1.24 \$	
17	F-1150	1650 17.063	3.10473F OL	-3.100445 04	-0.94 4	
14	Dr - 1-10	104 903.000	0.122-16 04	0.158*1F 05	14.77 *	
10	CL-46-44	12 116 1. 300	3.12005F ON	0.749536 03	0.41 %	
20	CC-8-67	134427.125	0.133716 Ce	-0.15070= 04	-1.19 €	
21	*13	F1614. 043	0.021376 35	0.917776 34	11.05 \$	
27	990	111527.125	D. IC. TIF Ce	-0.44114E 04	-5.87 4	
**	f-70	11047.016	J. 3/24 05 05	0.4 14 3AF 34	13.74 €	
24	PT-9-10	41491.077	0.455115 05	-0.379176 03	-0.76 T	
75	DC-9-10	55259.012	0.437ACE 04	-0.22011E 04	-3.42 \$	

5 . wat # 17.	VEHICLE 10.	INDIT VALUE	CALCULATED VALUE	oter.	****
11.	20-11-30	55051.004	2.51746[05	-0. 75F47F 04	-4.40 €
27	727-100	*******	7.77252E C5	-0.55454E C4	-4.75 3
**	7**-720	6, 577. 347	0. + 771 95 04	-3.11#74F 94	-3.43 T
20	737-126	*3 *00.073	A. 52373E C5	-0.1476PF 04	-7.75 4
?!	717-200	44074. 377	C. 4.27AE 05	0 . 14694F 04	2.69 \$
11	VC-12	141697.125	C.120141 CA	-0. 71 5776 65	-15.70 4
**	VC-125	14 120 3-125	7.141.4F JA	0.110525 05	7.01 €
**	6141-2	110141.125	0.17147E CF	-C. dn940F 04	-6.47 4
15	F-5A	227:07-125	7. 115-5F OF	0.84*14F 34	2.58 \$
36	00-10-10	274477.135	0.21813F Ce	-3.67914F 04	-2.90 4
17	747-27	727077.250	0.710-15 CA-	-0.12443F 05	-3.44 \$
34	741	313713.108	C. TIDALF OF	-0.76076F C4	-0.93 4
**	tle.t	215993. 363	1.23244F CA	C.14904E 05	7.41 8
40	C-141-1	127640.063	C.12167F 06	-0.50719F C4	-4.58 *

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